

FLUXLESS SOLDERING IN ACTIVATED HYDROGEN ATMOSPHERE

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ABSTRACT

A novel hydrogen activation technology based on activated hydrogen or electron attachment (EA) is developed for fluxless soldering at ambient pressure and normal soldering temperature. The technology has a potential to be used for a list of applications in the electronics packaging industry and recent work by a joint effort between Air Products and Sikama International on alpha trials of a production-scale furnace for flux-free wafer bump reflow based on electron attachment (EA).

Key Words

Fluxless soldering
Activated Hydrogen
Electron Attachment

INTRODUCTION

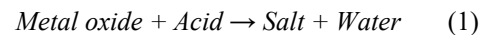
Packaging technology for electronics devices has advanced rapidly in recent years driven by feature size reduction, new materials development, and increased demand on device functionality. The most fundamental among the advanced packaging technology is the use of wafer bumping and wafer-level chip scale packaging.

In a wafer bumping process, fine-pitch electroplated solder bumps are formed over an entire silicon wafer on which integrated circuits have been built, the wafer is then reflowed at a temperature above the solder's melting point to complete metallic interconnection of the bumps with underneath metal pads and convert the bumps from a deposited shape into a ball shape. After the wafer bumping, the wafer is cut into individual chips, which then go through subsequent packaging processes. In the packaged devices, the formed bumps serve as electrical, mechanical, and mounting connections. Current study is related to the last step of the wafer bumping process — wafer bump reflow.

One of the keys for successful wafer bump reflow is to remove the native oxide layer and prevent additional oxidation on the bump surface. Any oxide layer on the bump surface will act as a solid skin to constrain molten solder's flow, which in turn causes a non-qualified bump appearance and non-uniform bump shape across a wafer. This oxide elimination is becoming more critical and

difficult as the bump size shrinks since the increased surface to volume ratio plus the enlarged surface curvature of the solder bump drives toward a more severe solder oxidation to minimize its surface energy.

Currently, the most common approach is to coat the wafer with a flux and then reflow the wafer in a nitrogen environment. The oxide removal capability is attributed to the organic acids in the fluxes (1).



However, such flux-containing reflow process is not ideal, since the decomposition of organic fluxes always leaves residues and generates volatiles, which invariably bring contaminants on the wafer and furnace walls. Therefore, a post cleaning of the reflowed wafer is always required. A frequent cleaning of furnace interior surfaces is also needed, causing high maintenance costs and a lot of equipment downtime. In addition, special safety precautions have to be taken for dealing with hazardous disposal of the flux residues and unhealthy exposure of the flux vapor. Besides the cost and inconvenience associated with the cleanings, the flux-containing process directly affects the quality of the reflowed wafer. For example, during reflow the flux can get into the molten solder and create voids inside the bumps, thus degrading mechanical and electrical properties of the solder joints in packed devices. As the pitch and bump sizes are continually decreasing, the need for process cleanliness increases. This has led to increased use of flux-free processing, which is mainly based on using a reactive gas to replace the organic flux for oxide removal.

However, known flux-free technologies all have different problems or limitations. By using formic acid vapor, the process is not completely residue-free and has to be operated in a sealed vacuum system. Hydrogen-based flux-free process is clean and non-toxic, but high temperature ($\geq 350^\circ\text{C}$) and pure hydrogen (flammable) must be applied to activate and hasten the oxide reduction. Plasma-activated hydrogen can make the oxide reduction efficient at low temperatures, but only vacuum plasma appears to be viable, resulting in a batch process.

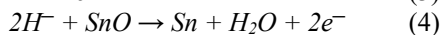
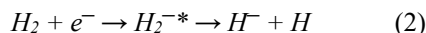
Therefore, our objective is to develop a novel hydrogen activation technology based on electron attachment (EA) for fluxless soldering at ambient pressure and normal soldering temperature using nonflammable mixtures of hydrogen (≤ 5 vol%) in nitrogen.

ELECTRON ATTACHMENT

Basic Principle

Electron attachment (EA) is defined as follows. When low-energy electrons, such as below 10 eV, collide with gas molecules, some are captured by gas molecules, producing anions by dissociative or direct attachment [1].

Equation (2) represents the dissociative attachment for hydrogen, where a hydrogen molecule (H_2) combines with an electron (e^-) to give an excited molecular hydrogen anion (H_2^{-*}) which dissociates to give an atomic hydrogen anion (H^-) and a neutral hydrogen atom (H). The neutral hydrogen atom can further capture an electron, forming an excited atomic hydrogen anion (H^{-*}) by direct attachment (3). The excited atomic hydrogen anion can be stabilized by releasing a photon or colliding with a nitrogen molecule. Nitrogen as the dilution gas is inert to EA because its electron affinity is close to zero. Driven by an applied electrical field, the atomic hydrogen anions formed under EA can be directed to the soldering surfaces for oxide reduction. Equation (4) is an example of reducing tin monoxide. As reduction by-products, water vapor can be easily vented out of the furnace and free electrons can be removed properly.



Process Establishment

Figure 1 shows an example of establishing EA in an open tunnel furnace typically used for reflow soldering. An electron emission apparatus containing a lot of sharp tips is mounted on the top side of the furnace. The furnace is purged with a nonflammable mixture of hydrogen (≤ 5 in nitrogen). Electronic devices to be soldered are loaded on a transportation system, which continually moves from the entrance to the exit of the furnace. When passing underneath the electron emission apparatus, the electronic devices will expose to the EA atmosphere. After EA cleaning of oxides on soldering surfaces, the devices will undergo the normal solder reflow and cooling.

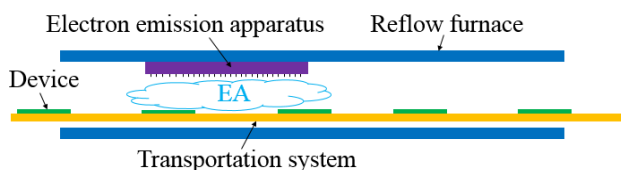


Figure 1. Establishing EA in a reflow furnace

A major challenge for achieving the proposed fluxless approach with EA was to generate a large quantity of low energy electrons under ambient pressure. There was no commercially available electron emitter that could satisfy the requirements for current application. Therefore, in our research we developed a patented technology for the electron emission apparatus. The apparatus contains own anode and cathode. With applying a pulsed DC (direct current) voltage in a range of 2 to 3 kV, electrons can be emitted out of the apparatus independently. In the case that soldering surfaces underneath the apparatus are isolated with ground and not able to drain charges, the apparatus has a capability to collect free electrons that accumulate on the soldering surfaces and still emit electrons.

Figure 2 shows an electron emission module with 3" X 3" in size. A number of such modules can be integrated together to scale up the electron emission. Figure 3 demonstrates a status of electron emission when the module is operated above an electrically insulated glass. By initiating a required electrical power, all the tips on the module are illuminated, which is mainly due to gas molecules surrounding tips are excited. The illuminated tip array is reflected on the glass surface.

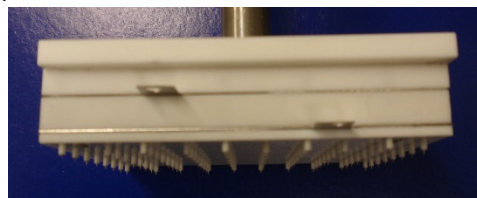


Figure 2. Electron emission module (3" X 3")

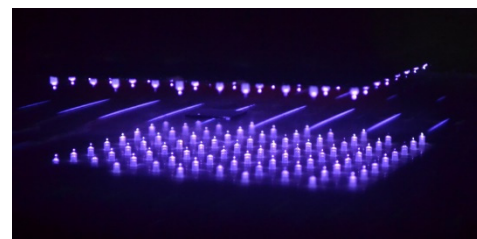


Figure 3. Electron emission on insulated glass

PROOF OF CONCEPT

Hydrogen Dissociation

The most fundamental theory of using EA to activate hydrogen is the dissociation reaction that forms atomic hydrogen anions [2]. We investigated this by using a mass spectrometer (MS) to detect hydrogen-deuterium (HD) formation in a furnace environment containing hydrogen (H_2) and deuterium (D_2) at 280°C. As shown in Figure 4, the HD intensity increased when EA was applied at $t = 15$ min, and returned to its original level after EA was stopped at $t = 25$ min. There were also corresponding changes for H_2 and D_2 intensities. This result confirms the dissociation of H_2 molecules under EA [2].

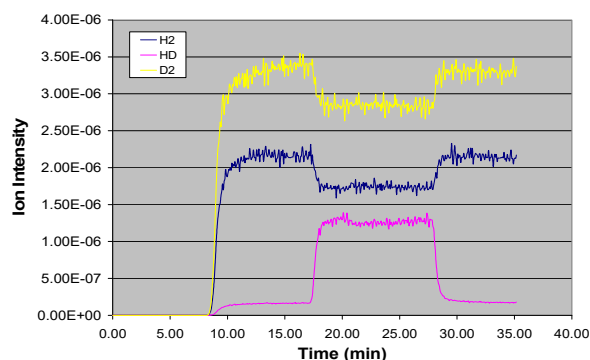


Figure 4. MS spectra showing reactions under EA

Solder Wetting

A fluxless solder preform in a pellet shape was put on a copper plate and heated up in 5 vol% H₂ in N₂ either with or without applying EA. Without applying EA, the molten solder maintained to be in the pellet shape (Fig. 5a). When EA was applied during heating, the solder spread out with a shiny surface (Fig. 5b). This experiment was repeated for different solders listed in Table I. In most cases, the temperature for each solder to wet was quite close to its melting point, thus demonstrating the efficiency of EA.



a) Without EA b) With EA

Figure 5. Effect of EA on solder wetting

Table 1. Solder Wetting Temperature under EA

Solder Composition (wt%)	Dominant Surface Oxides	Oxide Thickness (Å)	Melting Point (°C)	Wetting Temperature (°C)
63Sn/37Pb	SnO	30	183	197
90Pb/10Sn	SnO	30	305	306
96.5Sn/3.5 Ag	SnO	30	221	226
99.3Sn/0.7Cu	SnO	20	227	228
95Sn/5Sb	SnO	20	240	242
48Sn/52In	In ₂ O ₃	20	117	150

APPLICATION DEMONSTRATION

Wafer Bumping

Wafer bumping is used to form solder bumps over an entire silicon wafer before cutting it into chips. The formed bumps serve as electrical, mechanical, and mounting connections for flip-chip assemblies. A reflow process is used to metallurgically connect the deposited solder bumps with the solder pads and convert the deposited bumps into a spherical shape. Figure 6 shows tin-silver bumps on a wafer before and after reflowing. In the absence of EA, the reflowed bumps have surface collapse and uncompleted shape conversions due to a restriction of the oxide skin on the molten solder. Solder bumps reflowed under EA have a very smooth surface and spherical shape, indicating an oxide-free solder surface.

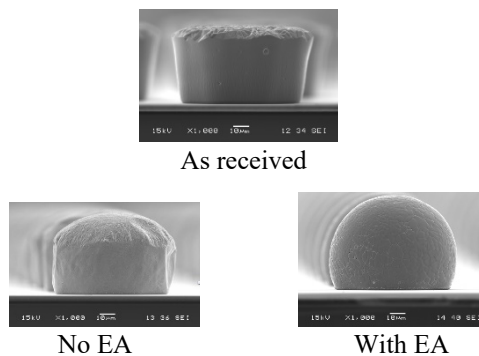


Figure 6. Effect of EA on solder reflow

CURRENT PROCESS STUDIES

Current study is related to a novel flux-free technology based on electron attachment (EA), which can be operated at ambient pressure and normal solder reflow temperatures using non-flammable mixtures of hydrogen (≤ 5 vol%) in nitrogen. The technology is invented by Air Products in recent years, which involves generating a large quantity of low-energy electrons. Some of the electrons can attach to hydrogen molecules, forming active species for oxide removal. The basic concept and the efficiency for oxide removal have been demonstrated in previous studies [4], [5]. The EA-based technology is completely residue-free and has a potential to be widely used in the electronics packaging industry. This paper presents a recent work between Air Products and Sikama International on alpha trials of an EA-enabled prototype furnace for production-scale wafer bump reflow (Fig. 7).

ALPHA TRIAL RESULTS

As shown in Figure 8, the EA-enabled furnace contains a roller-featured wafer transportation system, which carries wafers through heating and cooling zones with a standard production speed. Before entering a reflow zone, wafers are exposed to EA-activated 5% H₂ in N₂ for removing solder oxides (Fig. 9).

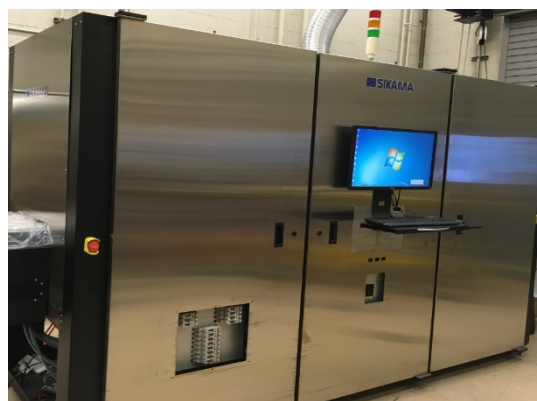


Figure 7. EA-enabled prototype furnace for production-scale wafer bump reflow

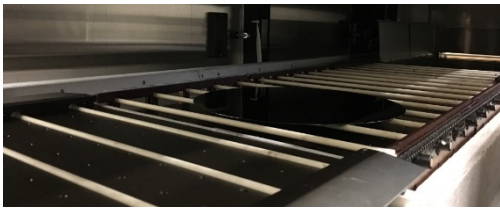


Figure 8. Roller-featured wafer transportation system



Figure 9. Wafer entering an EA zone for oxide removal

Various dummy wafers (8" and 12") with as-plated solder bumps were obtained from different customers and processed in the furnace to evaluate bump reflow quality. Figure 10 shows a cross section of a reflowed tin-based solder bump plated on nickel. The intermetallic compound (IMC) formation controlled by reflow time and temperature is quite acceptable. The effectiveness of EA on oxide removal has been clearly demonstrated in multiple trials. Figure 11 compares bump shapes of a lead-free solder on a wafer undergone different reflow processes. Before reflowing, electroplated bumps are in a cylindrical shape (Fig. 11a). Without applying EA in the H₂ and N₂ mixture, reflowed bumps have a rough surface and uncompleted shape conversion (Fig. 11b). With applying EA, reflowed bumps have a smooth surface and spherical shape (Fig. 11c), even better than that of flux-reflowed bumps after cleaning (Fig. 5d). As shown in Figure 12, the EA-based process can ensure a good bump uniformity across the width of a 12" moving wafer. In addition, the surfaces of the post-reflowed wafers are free of extra solder and foreign materials (Fig. 13).

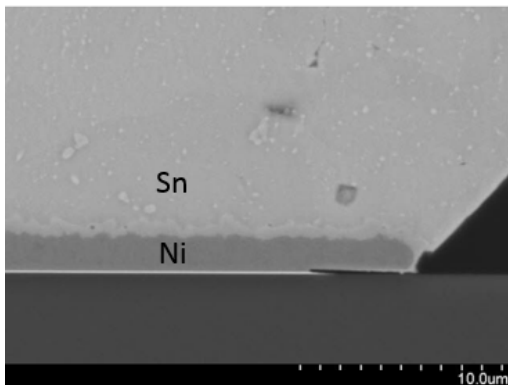
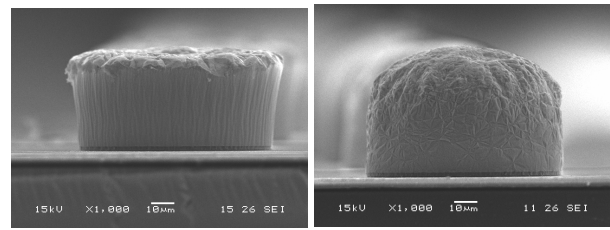
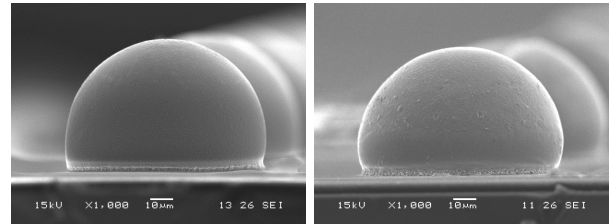


Figure 10. Cross section of the IMC



a) Before Reflow

b) Reflow without EA



c) Reflow with EA

e) Reflow with flux

Figure 11. Bump shape comparison

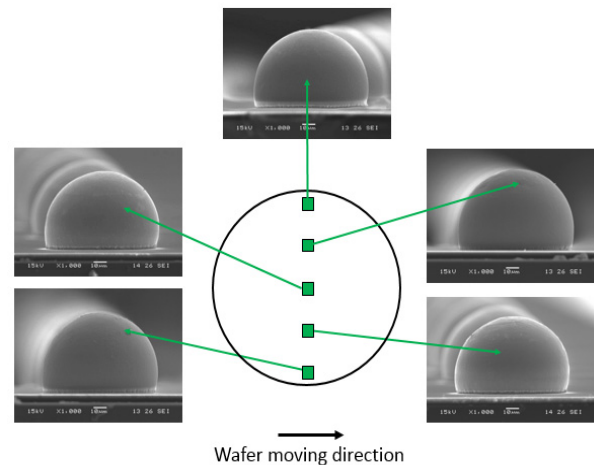


Figure 12. Uniform bump shape by EA-based process

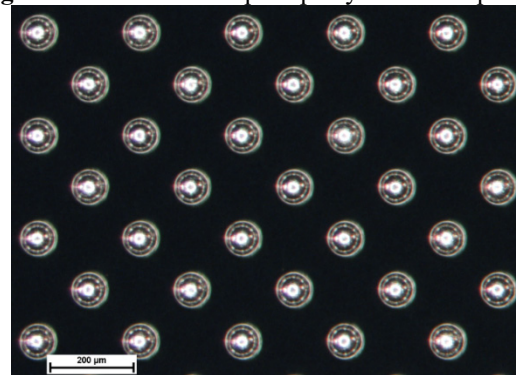


Figure 13 Clean wafer surface after EA-based reflow

Full dummy wafers reflowed in the EA-enabled furnace were also sent back to corresponding customers for standard quality inspections, such as checking bump shape, bump uniformity, shear strength, failure model, and bump voids. Results confirm that the wafers reflowed under the EA-based process indeed meet all specifications. Figures 14 and 15 represent results of automated optical inspection (AOI), which confirm acceptable bump heights (BH) and bump diameters (BD) across an 8" full wafer. Figure 16 shows that

all shear failures are within solder bumps and shear strengths well exceed the criterion ($> 2 \text{ g/mil}^2$). Figure 17 is an x-ray image of a die on a reflowed wafer, which demonstrates that the number of bump voids (green) is quite low and the size of a typical void is 3% of the bump area, which is much below the specified upper limit (8% of the bump area). [6]

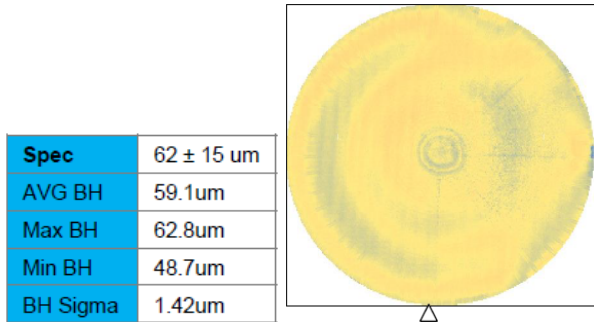


Figure 14. BH distribution map and data

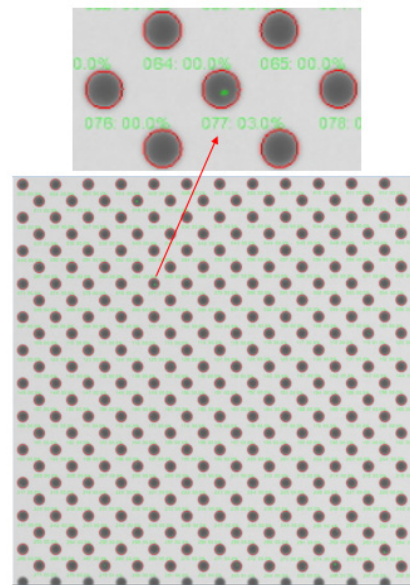


Figure 17. X-ray image of a die

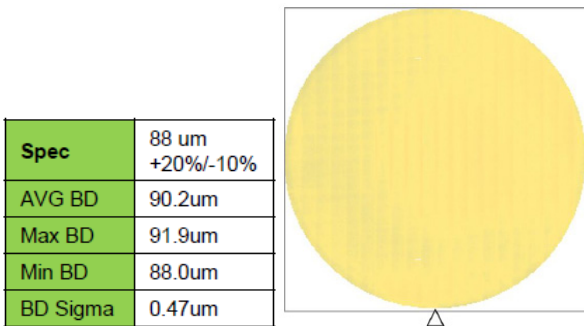
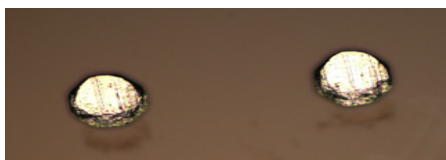


Figure 15. BD distribution map and data



AVG	Max	Min
3.70	4.11	3.34

Spec > 2 g/mil²

Figure 16. Bump shear failures and data

ELECTRICAL EFFECTS

The use of low energy electrons to activate the hydrogen molecule to form hydrogen anions has been a subject of debate on possible damage to a functional device or wafer. With our generation of these low energy electrons from the emitter systems the key to reduce the buildup of charge on the isolated, non-grounded wafer is eliminated by the emitters capability to pull back the electrons off the surface of the wafer.

To demonstrate that this pull back of the electrons by emitters was in fact occurring, several tests with active wafers, first level integrated circuits and Known Good Die (KGD) were conducted.

The initial test group were thirty (30) TI OPA 2333 CMOS operational amplifier Known Good Dies (KGD) purchased from Micross who also provided the post testing analysis. Figure 18 shows the KGD as received.

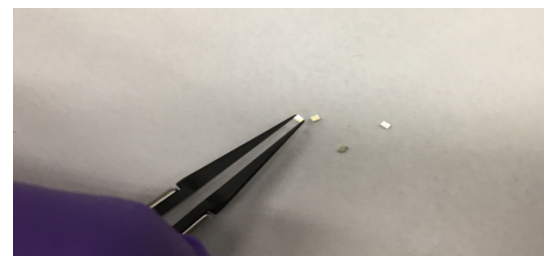


Figure 18. TI OPA 2333 KGD

The KGD were placed onto a blank silicon wafer that was machined to hold the dies in place as they were passed through the EA reflow furnace. The 30 KGD were exposed to the low energy electrons based on the process parameters used for the bump and copper pillar reflow test as above. The KGD were sent back to Micross for post EA analysis and their final analytical report concluded that there was no damage to the functionality of the Known Good Dies.

The second test group was done at the transistor level and was a SRAM chip at the 28 nm mode and provide by integrated circuit foundry house. Figure 19 shows the first device at the contact level.

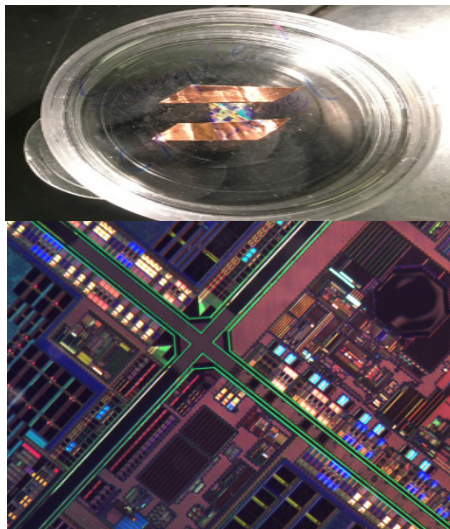


Figure 19. Die 1 at Contact Level

A device at the metal level was also tested as shown in Figure 20.

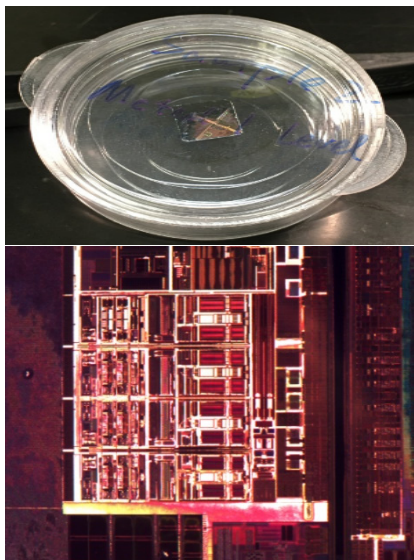


Figure 20. Die 2 at Metal Level

These functional level devices were run through the EA reflow furnace based on process parameters used for the bump and copper pillar reflow tests.

As shown in Figures 21 and 22, the IV curves ($I_d - I_v$), the overlay of the pre and post EA curves are closely matched. For both the PMOS and NMOS, the average change in the I_{d-lin} , I_{d-sat} , V_{t-lin} and the V_{t-sat} parameters are within 5% for all the transistors tested and these were acceptable results as tested and concluded by the foundry that supplied the devices.

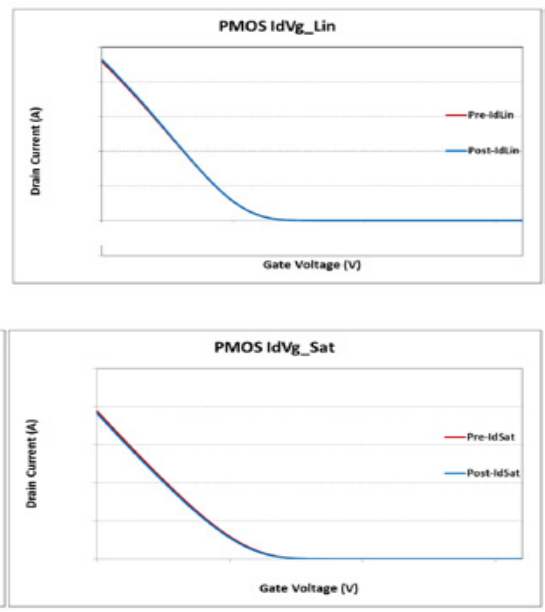


Figure 21. PMOS Curves

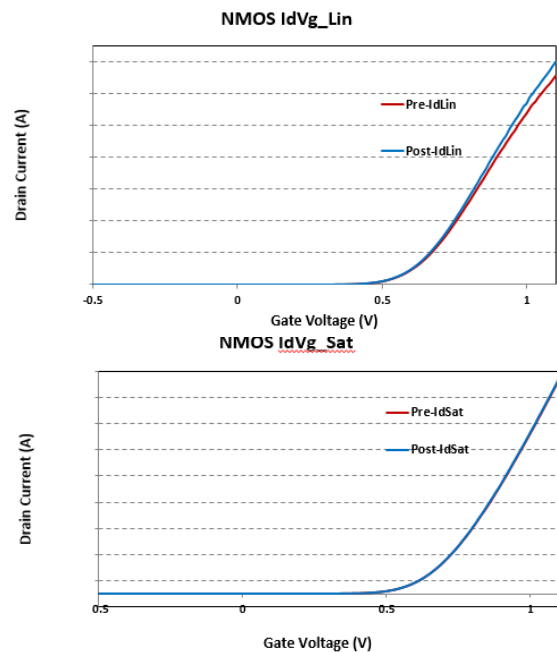


Figure 21. NMOS Curves

The final test group involved fully functional eight-inch (200 mm) CMOS wafers from a major semiconductor company. Two probed wafers were processed in the EA activated hydrogen reflow system with the same parameters as the previous tests. Pre and post probe testing was completed by the major semiconductor company that supplied the wafers. Post EA processed probe testing showed insignificant changes to the device characteristics as compared to the pre-EA process data.

From the three test programs above, we can conclude that the EA activated hydrogen process had no effect on the electrical characteristics or functionality of the devices on the wafers.

CONCLUSIONS

Trial results demonstrate that dummy wafers reflowed in the EA-enabled production-scale furnace meet customer specifications. The EA-based technology offers the following benefits for wafer bump reflow: 1) enhanced bump reflow quality because the flux induced solder voids and wafer contaminations naturally disappear, 2) improved productivity by having in-line process capability, eliminating post wafer cleaning, and avoiding furnace down time cleaning, 3) reduced cost of ownership due to eliminated costs associated with cleaning equipment, solution, labor work, and flux, 4) improved safety by eliminating flux exposure and using a non-toxic and non-flammable gas mixture, and 5) no environmental issues by eliminating organic vapors, hazard residues, and CO₂ emission. Through the testing to observe the effects of the low energy electrons, EA activated hydrogen process had no effect on the electrical characteristics or functionality of the devices on the wafers.

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